#### **MECH5080M – Team Project**

# **Developing the transmission system of an active stability system of a sounding rocket**

MECH5080M Team Project – Individual Report *Improving an active stability system of a sounding rocket Author: Antoine Durollet - 201439724 Supervisor: Jongrae Kim Industrial Mentor: Theo Gwynn Examiner: Robert Kay Date: 30/04/2024*



MECH5080M TEAM PROJECT 45 credits

TITLE OF PROJECT

Developing the transmission system of an active stability system of a sounding rocket

PRESENTED BY

Antoine Durollet

OBJECTIVES OF PROJECT

Develop a transmission system for an active control system, and oversee the flight simulations of the rocket.

IF THE PROJECT IS INDUSTRIALLY LINKED TICK THIS BOX



AND PROVIDE DETAILS BELOW

COMPANY NAME AND ADDRESS:

Airbus Defence and Space

Gunnels Wood Rd, Stevenage SG1 2AS

INDUSTRIAL Mentor:

Theo Gwynn

THIS PROJECT REPORT PRESENTS OUR OWN WORK AND DOES NOT CONTAIN ANY UNACKNOWLEDGED WORK FROM ANY OTHER SOURCES.

SIGNED  $Arb_1$  DATE 30/04/2024  $\Lambda$ 

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### <span id="page-4-0"></span>**Abstract**

This paper goes over the research and work that was carried out to develop the transmission system of an active control module for a sounding rocket. The main objective of the report is to detail how the transmission was designed and ensured to be sturdy enough to handle the constraints of a rocket flight. It outlines how the shape of the canards was chosen using both simulations and testing, how the transmission was designed and implemented, and goes over the flight simulations of the rocket and compares them to the data obtained during the flight.

# <span id="page-5-0"></span>**1) Introduction**

#### <span id="page-5-1"></span>a. Introduction

The Aptos project was started in 2022 in order to develop an active control system for a sounding rocket. The reason it is needed is because when rockets fly, they tend to point their nose into the wind, this phenomenon is called weathercocking, and causes the rocket to have a lower apogee. To counteract this, a system composed of variable angle aerofoils, called canards, was implemented.

The Aptos project is done in conjunction with the Leeds University Rocketry Association (LURA) and aims to develop an active control system and use the findings to incorporate into the future rockets of LURA. LURA aims to be a pioneer in developing new rocketry technologies and push the current knowledge of rocketry further. To achieve those goals, LURA has set itself the long-term objective of reaching the Karman Line, the arbitrary line where space begins, which is at 100km of altitude. Currently, no UK university team has been able to reach this altitude. The current rocket, the Gryphon II, is aimed to break the current amateur rocketry record, held by the University of Sheffield and set at over 11 km, by going to 13 km. Its successor, the Gryphon III, is planned to reach an altitude of 50 km, the halfway mark to the Karman Line.

<span id="page-5-2"></span>b. Background

The previous year's team had designed a transmission system onto which the canards were directly mounted on the servomotors, which caused damage to the servomotors when the rocket landed during their first test flight in April 2023. There was also a problem that the canards could come undone easily and the entire system had to be disassembled to be able to mount the canards back in place. Another problem that existed was that there was a space between the radial holes for the canards and the canards mount points, which ended in the servomotors taking most of the weight of the canards and the loads caused by the rocket flying in the air.

#### <span id="page-5-3"></span>c. Aim

The aim of the project is to work on and improve an already existing active control system for a rocket to implement in the future rockets of the Leeds University Rocketry Association.

#### <span id="page-6-0"></span>d. Objectives

The objectives of the aerodynamics team were to develop a new canard shape, create a new transmission system and oversee the simulations and design the various parts for the test flights.

#### <span id="page-6-1"></span>e. Report Structure

This report will go over each of the objectives and how they are achieved. It will first go over the existing literature for active control systems and canards in rocketry, then will go in depth on how the shape and planform of the canards were selected. After that, it will talk about the transmission system that was implemented and the testing required for it to fly. It will then summarize the results from the launch that was conducted on the  $14<sup>th</sup>$  of April 2024.

### <span id="page-7-0"></span>**2) Literature Review**

To ensure that a rocket will fly straight, it needs to be stable. This is done by creating a rocket such that the centre of pressure is aft of the centre of mass. This is so that the aerodynamic forces acting on the rocket keep it aligned with the airflow. The ratio between the two is called stability calibre [1], and the generally accepted static margin is  $SM > 1$ . It is achieved by modifying the size of the aft fins and shifting the weight inside the rocket.

A passive stability is not always desired, especially in the case of high-altitude flights. Passively stable rockets tend to weathercock when there is a cross wind, which results in a lower apogee than expected and a larger landing area [2]. For that reason, an active control system is usually preferred for high altitude flights as it controls the dynamic stability of rockets and allows unstable rockets to fly pre-determined trajectories and modify them.

There are different types of active control systems [3], the most known being aerodynamic control surfaces, which are similar to what is currently used on airplanes, gimballed engines, which is seen on the bigger rockets from NASA, ESA and SpaceX. The third type is using canards at the fore of the rocket. The canard method was chosen as the rocket bodies are quite small and the first two systems take too much space near the aft of the rocket, where the motor is.

The aerofoil can have multiple chord shapes [4] [5]. Out of the existing ones, the straight tapered wing was favoured as its shape reduces the vortex on its tip, resulting in a lower drag than a constant chord wing. It is worth noting that a tapered wing is less efficient than an elliptical-shaped wing but is easier to manufacture. It was also decided to have a straight swept aerofoil [5] as the rocket was estimated to have a maximum velocity of 103m/s or M=0.311. Swept wings are more common and see their advantages increase exponentially as the speed gets closer to the speed of sound, at 330m/s.

A four-digit NACA aerofoil was chosen as they usually have a softer stall than higher NACA types. They also have a more gradual increase in drag as the lift increases, meaning that they provide a higher lift to drag ratio [5]. All of this makes NACA four-digit aerofoils more permissive of errors which makes them the better choice for a first design.

The aspect ratio is an important factor to consider when designing an aerofoil. A higher aspect ratio makes the airflow be closer to a 2D airflow, which creates no induced drag meaning that a higher aspect ratio increases the lift coefficient and decreases the drag

coefficient [6]. However, a high aspect ratio will also increase the bending stress and will start to have torsion if the aerofoil is too long. They also have slower roll rate and acceleration than aerofoils with smaller aspect ratio [7].

The load transmission is being done by a shear pin. To ensure the pin doesn't shear under a certain load, the bearing stress equation has been used [8]. This takes into account the shape of the pin, as well as the thickness of the plate and the load.

Polylactic acid (PLA), is a thermoplastic acid that is often used in fused deposition modelling (FDM), also know as fused filament fabrication (FFF). PLA is a biodegradable plastic that has a high versatility, is relatively low cost and highly accessible [9]. It's easy accessibility and low cost allows to create multiple versions of a part or system in a relative short time through the use of FFF printers such as the Bambu Lab printers. It is a material that has a low melting point, around 160°, and doesn't shrink much when cooling, its thermal expansion coefficient is around 73 μstrain/°C, which allows it to keep the shape of the part accurately [9].

# <span id="page-9-0"></span>**3) Defining the Canards**

In order to define the optimal aerofoil, the CFD software XLFR5 was used as it was developed specifically for aerofoils simulation. The aerofoil needed to be symmetrical as it needs to provide no lift when in neutral position while being able to provide lift at both positive and negative angles. A range of NACA aerofoil shape were simulated, from NACA 0010 to NACA 0020.



*Figure 3.1. CFD Comparison of three NACA Aerofoils*

<span id="page-9-1"></span>The three best aerofoil shapes were found to be NACA 0014, NACA 0015 and NACA 0016. The latter was chosen due to its slightly higher stall angle and higher coefficient of lift. It can also be seen from the second graph that the stall angle of the canard is at 16.5°.

The planform of the canard was dictated by two main factors. The first one, which required to make the canard larger, being the corrective moment [10] [11] required to steer the rocket in the air without requiring too high of an angle of attack. The second one, which aimed to reduce the size of the canard, was the drag created by the canards, and drives the centre of pressure closer to the centre of mass, making the rocket less stable. To help in this task, an excel spreadsheet was created.



*Figure 3.2. Dimensions of a tapered aerofoil*

<span id="page-10-0"></span>After modifying the different lengths of the canard, the root chord was chosen to be  $a =$ 80mm, the tip chord would be  $b = 50$ mm and the wingspan would be  $h = 70$ mm. This gives the canards an aspect ratio of 1.077 [7]. This is to ensure that the canards do not experience too much bending stress and break away from the rocket.

The estimated lift force required to provide the desired corrective moment is 103.565 N for a cross windspeed of 10m/s. This force generates a pitching moment of 0.483 Nm about the canard.

To confirm the results from the simulations, a wind tunnel test was carried out using the wind tunnel of the ESTACA engineering school.

# <span id="page-11-0"></span>**4) Transmission System**

Due to issues that arose in the first version of the transmission system, it was decided to create a second version. The first idea was to have a bearing put in place to help alleviate the servomotor, and the second was to prevent the forces caused by the ground acting on the canards when the rocket lands to reach the servomotors. Figure 2 shows how the previous system attached the canards to the servomotors, while Figure 4 shows the new system



that was designed to answer the issues that were met in the first design.

#### *Figure 4.1. Previous Aptos Module Transmission System*

<span id="page-11-1"></span>To solve the first problem, it was first envisioned to use ball bearings. However, because of their thickness it prevented the canards to be connected to the servomotors. This meant that the other choice was then decided to use brass bushings, which was chosen.

To prevent the canard from moving past its stall point, which would reduce in a sharp decline in lift, and hence rotational moment, a slot has been cut into the bushing to limit the range to +/-15°.

<span id="page-11-2"></span>

*Figure 4.2. Brass Bushing*

To reduce the drag created by it, they were also filed down to the outer diameter of the rocket as closely as possible.

The second issue was solved by redesigning the whole transmission. To begin, a shaft was designed to be mounted on the servomotor using 4 centering pins and a bolt to secure it in place.

The attachment point of the canard to the shaft was set so that it would be fore of the centre of pressure. This is so that if the shear pins broke, the canards would automatically come to their neutral position with an angle of attack of 0°. This is so they will not create any lift and modify the roll, pitch or yaw angle of the rocket.



To assemble the transmission system, the servomotors (4) are mounted into a 3D printed bed (2) and are secured in place with the 3D printed lid (3). This sub-assembly is then slid inside

Figure 3.2. Exploded View of the Aptos Module

the Aptos module (1). Once it is in place,, the shaft (6) is connected to the servomotor, and secured in place using a bolt (7). The canard (8) is then mounted on top of the shaft and connected to it using the shear pin (9). The brass bushing (5) has been glued prior to the assembly to take the brunt of the axial load from the canards, and to ensure that the frictional losses are kept to a minimum.

Once the shaft is installed on the servomotor, the canard can be mounted on it and is secured in place using a shear pin made of anycubic resin [12]. The shear pin is design to transfer the load from the servomotor to the canard and break when the rocket lands on one of the canards, so that it does not damage the servomotor.

Anycubic resin was chosen as the tolerances in the canard and shaft are low to prevent the canard from moving on its own. By using anycubic, a flexible material, it allows to insert the pin without breaking the part while locking the mechanism in place.

The dimensions of the pin were calculated by estimating the impact force the canards will undergo.

$$
F_{impact} = ma_{impact} = m \frac{v_{impact}^2}{d_{impact}}
$$

Where the mass of the rocket is 8.392kg, its ground hit velocity is 5.67m/s and the estimated duration of impact is 0.3m due to the soft nature of the ground and the crops that would soften the landing.

Once this was found, the torque this force generates about the canard is:

$$
T_{impact} = F_{impact} * d
$$

Where the distance is the length from the aft of the canard to the centre point of the shaft hole.

From this, the force acting on the shear pin can be calculated using the torque.

$$
F_{shear} = \frac{T}{d_{pin}}
$$

After finding the forces going through the shear pin, the bearing stress the pin will undergo was calculated.

$$
B_t = \frac{F_{shear}}{t_{plate} * D_{pin}}
$$

The bearing stress generated when the rocket lands is estimated to be 1.179 GPa. The flexural strength of the material is 50-60 MPa according to the manufacturer [9], which would result in a breaking torque of 1.162Nm This means that the shear pin should break when the rocket lands. However, as the maximum torque the servomotors should produce is 0.48 Nm, which is comparable to a stress of 11.364 MPa, the shear pin should manage to transfer the load to the canards without breaking, and break upon landing.

The servomotors that were used in the previous year had to be changed. This was decided during a meeting with the United Kingdom Rocketry Association (UKRA), the governing body of amateur rocketry, where the transmission mechanism of the servomotor was discussed. The previous servomotors, the Herkulex DRS-0101 [13], uses plastic gears, and they felt more comfortable with a servomotor that uses metal gears. As the rest of the system was already designed and had started manufacturing, it had to follow the electronical requirements of the previous servomotor. Specifically it had to have an UART protocol communication system, and a rated .current of 7.4V, while having a stall torque equivalent or higher to it. The dimensions of the new servomotors also had to be as close as possible to that of the previous ones to fit inside the Aptos module. After establishing those requirements, a suitable servomotor was researched and selected. The chosen servomotor selected by both the avionics and aerodynamics team was the STS 3215 [14]. This servomotor uses copper gears, has a stall torque of 19 kg.cm, or 1.9 Nm, which is higher than the Herkulex-0101, and uses an asynchronous serial communication protocol.

# <span id="page-14-0"></span>**5) Testing**

The wind tunnel testing was carried out at the ESTACA engineering school in France [15] as there were problems with the wind tunnel in the University of Leeds. In addition, the wind tunnel at the ESTACA can go to 40m/s [16], whereas the wind tunnel at the University of Leeds can go to 12m/s. The wind tunnel that was used utilizes a force balance system, similar to the one used at the University of Leeds. It was carried out using 3D printed canards and by having a set of two canards mounted on both sides of the mount block to provide symmetrical lift and drag forces. A total of four different sets of canards were created, all at different angles of attack ranging from 0 to 15° with a 5° deflection between them. They were printed with the leading edge facing down. This was done to minimize the amount of supports while not making it too fragile during printing.

Each canard jig was tested three times, and the results were combined to have an average of the values given. The tests consisted of having a jig installed and the windspeed were gradually increased in increments of 5 until it reached the maximum velocity of 40m/s.

<span id="page-14-1"></span>

*Figure 5.1.1. Wind Tunnel of the ESTACA*



*Figure 5.2. Comparison of the Cl between the simulations and Wind Tunnel*

<span id="page-15-0"></span>The coefficient of lift generated by the aerofoil is lower than the simulated one, with a maximum discrepancy of 25.850% when the angle of attack is at 15°. The measured coefficient of lift is lower than the simulated one.



*Figure 5.3. Comparison of the Cd between the simulations and Wind Tunnel*

<span id="page-15-1"></span>It can be seen that the coefficient of drag between the simulations and the wind tunnel testing has the highest discrepancy at 37.872%, when the angle of attack is 0°.

When the wind tunnel is run at 40m/s [16], the lift force's slope starts decreasing starting at 10° while the drag force increases exponentially. This can be explained as the angle of attack gets closer to the stall point of the canard.

The differences between the simulations and the wind tunnel testing may be caused by the print orientation, and print quality which was set at fine where the nozzle diameter is 0.4mm. The combination of both could cause disruptions in the airflow, ending in a lower lift coefficient and higher drag coefficient as the shape of the aerofoil is not exactly the same.



*Figure 5.4. Comparison of the different AoA at different windspeeds*

<span id="page-16-0"></span>As the windspeed increases, the lift and drag force increase exponentially. It can be noted that at higher angles of attack, the lift force increases at a higher rate than the drag force. This means that as the angle of attack increases, the more efficient it becomes, until it reaches its stall point.

During the first assembly of the system, the servomotors were told to move past the 15° limit to see what would happen, and the shear pins broke. This ensured that they would break when the servomotors were moving past the  $+/-15^{\circ}$  range the bushings allow.

### <span id="page-17-0"></span>**6) Test Flight**

The Pathfinder rocket was flown on the 14<sup>th</sup> of April 2024 with the Aptos module installed. The UKRA, gave their approval to fly the rocket with the system enabled.

The flight simulations of the Pathfinder rocket were carried out with different windspeeds. As the position of the canards cannot be changed throughout the flight, they have been set at a 0° angle of attack for all windspeeds. The apogee is estimated at 462m above ground level, and the rocket has a passive stability of 1.81cal.



*Figure 6.1. Comparison of the OpenRocket model and flight data*

<span id="page-17-1"></span>The rocket flew to an altitude of 354m above ground according to the flight computer onboard. After the rocket landed and was recovered, it was noted that there was no damage to the canards and the shear pins did not shear. This could be because the calculations were taken with a high margin of security to prevent the pins from shearing during

<span id="page-17-2"></span>

*Figure 6.2. Aptos module after landing*

flight, which would cause the canards to fall off and prevent the trajectory to be corrected. This would also cause debris to fall which might hit and injure someone. As a secondary measure, the shear pins were glued in place to have a redundancy in case of one or multiple shear pins broke.

This discrepancy between the OpenRocket simulations and the flight data that was recovered could be caused by the software not being designed for active stability systems.

In order to simulate the aerofoils, a set of fins resembling as close as possible the shape of the canards was added to the Aptos module. However, they do not represent the real shape of the canards. The fins are also passive, meaning that they have a set cant that cannot be modified during the flight.

After gathering and comparing the data between OpenRocket and the flight, more simulations were run by setting the cant of the canards at different angles and it did not seem to impact the flight except in one case, where the canards are all set at the same angle, which creates roll and makes the rocket more stable, allowing it to reach a higher apogee.

# <span id="page-18-0"></span>**7) Conclusion**

### <span id="page-18-1"></span>a. Conclusion

The previous year team's system was functional but had some issues that had to be addressed. Primarily, the canards were mounted directly on the servomotors, which would cause damage to the servomotors when the rocket landed. Also, it had a tendency to easily undo itself, which would be a problem if it happened when the rocket was in flight. Another issue that existed was that to allow the canards to rotate freely, they were designed to not touch the bores. This forced the servomotors to hold the weight of the canards, as well as the aerodynamic forces acting on them, which causes them to get damaged faster. For these reasons, it was decided to review the whole system.

The canards were simulated using a CFD software designed for aerofoils, called XLFR5, and the results between last year and this year were compared. The entire canard was redesigned to produce more lift while having as little impact on the drag as possible. This resulted in a canard with a very low aspect ratio to minimize the bending moment. Once this was done, a model was made of the canard and was sent to the ESTACA engineering school in France to undergo wind tunnel testing at different angles of attack. The results of the simulations and tests have been compared and it came up that the lift generated in the wind tunnel was lower than the expected one from the simulations, while it produced higher drag forces. This could be caused by the printing parameters of the parts. Due to this, the orientation of the canards was modified so that they would be printed from the tip to the chord. This was done so that the print layers would help guide the airflow and not disrupt it.

The differences between the simulated and actual flights could be coming from inaccuracies from the software as it is not made to simulate aerofoils in that way.

The revised transmission system, being a first prototype, is designed to transfer a higher torque than is required. This was done to ensure that it did not break away during flight which would cause the rocket's trajectory to not be modified, and to prevent debris from falling off. However, as there was still a risk of them breaking off as they were not tested, it was decided to use superglue to hold them in place and reduce the chance of the canards from falling. The brass bushings that were designed were cut by hand, and therefore have a high tolerance in the slot.

### <span id="page-19-0"></span>b. Future Work

The next steps of the projects would be to improve on the transmission system, by preventing the canards from detaching in case of the pin breaks. Further wind tunnel testing could be carried out at higher speeds to better match the expected maximum speeds.

Future work should also focus on creating a mathematical model of the aerofoil to help the development of future canards, as well as increase the accuracy of the simulations, or even begin a software that is able to simulate the flightpath of rockets using active control.

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# <span id="page-22-0"></span>**9) Appendix**



### Appendix 1.Table for determining the canard shape

Inputs			Landing Inputs			Forces acting on APT Module		Shear on Impact from simulation		Shear from Servo	
							T impact	23,242636 Nm	Torque	0.48 Nm	
apogee	507 m		E kin	147.4992 J	E pot	130.0739 J	F pin	3265.506 N	F_pin	40,000 N	
distance_apt-aft	$1.445$ m			F_impact_ 520.2792 N		v impact 5.324556 m/s	<b>Bearing Stress</b>	927.701 MPa	Bearing <sub>S</sub>	11.364 MPa	
distance canard servo	$0.048$ m			F impact 425.8765		F_impact_ 484.2216 N					
Ground hit velocity	$5.67$ m/s					T_impact 20.44207 Nm					
Weight	9.176 kg							Material			
Gravity	$9.81 \text{ m/s}^2$						Anycubic Resin				
t_coll_est	0.1 s						Yield Strength	55 Mpa			
d_impact	0.3 <sub>m</sub>						<b>Tensile Strength</b>	55 MPa			
length half-shear-pin	6.26 mm	$0.00626$ m					Max Force	96.8 N			
thickness canard	1.76 mm	$0.00176$ m					Max Torque	1.1616 Nm			
D_pin	2 <sub>mm</sub>	$0.002 \, m$									
D servo	24 mm	$0.024$ m									
		<b>Flight Data</b>									
	Time Height	<b>Fall Speed</b>									
	314,612 13,263	5.27704437 m/s									
	68.182 24.802										

Appendix 2.Table for determining the Shear pin dimensions



Appendix 3. OpenRocket simulation with the canards at a 0° cant



Appendix 4. OpenRocket simulation with the canards at a 15° cant



Appendix 5. Sliced view of the shaft before 3D printing



Appendix 6. Sliced view of the canard before 3D printing

$\equiv$ File $\sim$ D. A				<b>Aptos Print Plates</b>			$x + y = 0$ $\overline{\phantom{a}}$
$\ddot{\mathbf{r}}$ <b>O</b> Prepare	<b>Pa</b> Device <b><i><u>■</u></i></b> Preview	<b>Project</b>	<b>Pa</b> Calibration		<b>J</b> Upload	Slice plate	$\sim$ Print plate
<b>D</b> Printer	$\circledcirc$				$\land$ Color scheme	$\sim$ Line Type	
Bambu Lab P1S 0.4 nozzle	$\mathbb{Z}$	圃			Line Type I Inner wall	Time Percent 28s 4.7%	Display 窗
- Textured PEI Plate Plate type		<b>MEDITER</b> o es			<b>B</b> Outer wall	1m47s 17.5%	W.
					Gap infill Support interface 39s	22s 3.7% 6.4%	<b>RE</b> 夏
<b>80 Filament</b>	思 $\langle \hat{0} \rangle$ $+$				<b>B</b> Custom	6m2s 59.1%	丽
1 - Bambu Support For PLA	$\alpha$	$\circ$			Travel Retract	1m8s 11.1%	面 百
					Unretract		贾
<b>Process</b> Global Objects	Advanced <b>D</b>				Wipe <b>B</b> Seams		量 展
$-$ * 0.12mm Fine @BBL X1C	099				<b>Total estimation</b>		
Quality Strength Speed	Others Support				Filament	$0.18 m$ $0.56 q$	
rop surrace pattern	EXYPROTOTOTIC				Cost Prepare time:	0.04 5m47s	
Top shell layers	$\hat{5}5$				Model printing time: 4m26s <b>Total time:</b>	10m14s	
Top shell thickness	0.6 mm						
Bottom surface pattern	Monotonic						
Bottom shell layers	$\hat{S}$ 5						
Bottom shell thickness	$\mathbf 0$ mm						
Internal solid infill pattern	Rectilinear						1.04
Sparse infill							
Sparse infill density	15 $\tilde{\mathcal{N}}$						
Sparse infill pattern	SGrid						
Length of sparse infill anchor	$-400\%$ mm or %						
Maximum length of sparse infill anchor	$\sim 20$ mm or %						
Advanced							
Infill/wall overlap	15 $\mathcal{H}_\mathrm{c}$						
Infill direction	45						
Bridge direction	$\mathbf{0}$						
Minimum sparse infill threshold	15 $\text{mm}^{\text{p}}$						
Infill combination	$\Box$				New network plug-in available Datails		0.20 $\times$
Detect narrow internal solid infill	$\overline{\vee}$						
Ensure vertical shell thickness					048		$\circledast$

Appendix 7. Sliced view of the shear pins before 3D printing











**Supervisor signature**<br>Jonyer/*i* 





![](_page_33_Picture_169.jpeg)

![](_page_34_Picture_122.jpeg)

![](_page_35_Picture_202.jpeg)

![](_page_36_Picture_217.jpeg)

![](_page_37_Picture_177.jpeg)

![](_page_38_Picture_119.jpeg)

![](_page_39_Picture_176.jpeg)

![](_page_40_Picture_190.jpeg)

![](_page_41_Picture_242.jpeg)

![](_page_42_Picture_218.jpeg)

I esting of assembly on (Thursday)

**Supervisor signature**<br>Jonyer *flix* 

![](_page_43_Picture_224.jpeg)

![](_page_44_Picture_311.jpeg)

#### **Agenda**

• Updates

• Launches

#### **Progress since last meeting**

Antoine:

• Wind Tunnel testing meeting with Sam. Going to be a few more weeks as they are testing a new equipment. Need to put pressure on Sam to do it asap.

Ollie:

- Will work with Sam to get the code working and changes needed to adapt legacy code to our new boards.
- Gyro data is pretty good.
- Accelerometer on the IMU is working.
- Tried to figure an angle from the axis of gravity. However, it uses the arctan function, which needs floating points that we don't have. Gives an approximate, but not close enough.
- Missing the BME280 and the servo drivers.
- Needs to do servo driver, BME driver and arctan problem.
- Might do low pass filters, but the data we get is good enough.
- Will check if the boards can fit horizontal in Aptos.

Alex Monk:

- Tried to demodulate the signal, but there is a lot of noise. Maybe the data rate is not correct? Not using an impedance match, so might have an impact.
- Need to try using a standard antenna to see if the problem isn't his antenna.
- Once demodulation is done, need to find a way to automatically read the data coming from the antenna. Need to copy the binary code from antenna into a .txt file before decoding by hand.

#### Alex Posta:

• Has been a bit ill. Poster has been submitted

Sam:

- Looked at the formulas for MATLAB and went over the code from last year to see what needs to be improved. Can't currently do floating points, which could be a problem for gains.
- Will work with Ollie to get the code working and changes needed to adapt legacy code to our new boards.
- Legacy was doing comms using Bluetooth. Getting rid of it and coming with an alternative solution to that.
- Need to work on servo drivers, and update controls from the Legacy.
- Need to implement changes of the updated Pathfinder to the simulations.

#### **Key notes**

- Servos are on their way to uni, and bushings are already here, waiting to be picked up.
- Launches:
	- $\circ$  G2 team to do launch on the 14<sup>th</sup> of April from MRC.
	- $\circ$  Can go to EARS on the 7<sup>th</sup> to do a test launch, do a small bottle test in the field?
	- o Test telemetry in a car?
	- $\circ$  Can put it on a drone and fly it. Sam has a drone. Can test on Sam's commercial drone.
- People will be back before the 14<sup>th</sup>, but not too sure how long before. Can go to Peak District on the  $5<sup>th</sup>$  to do testing.

#### **Actions for next meeting**

#### **Supervisor signature**

Donyer His

![](_page_45_Picture_153.jpeg)

![](_page_46_Picture_230.jpeg)

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#### **Actions for next meeting**

Oliver:

• Verify the servo positions before leaving

Alex Posta:

- Get Ollie's code working to see the canards moving
- Test the controller on microprocessor, and using the loop in Simulink
- Get floating point to work

Sam:

• Need to check that modifications make sense, and are the correct representation of how it will be simulated. More testing and experiments

Antoine:

- Need to finish prepping all the parts and assemble them together. Will be done by Sunday morning
- Need to find an alternative for the wind tunnel. (IPSA? Need to ask one of his old teachers.) Alex Monk:
	- Get the oscillator going. Take out all the wrong decode/noise data
	- Modify the PCBdesign
	- Buy a new antenna

#### **Supervisor signature**

Donyer His

![](_page_48_Picture_197.jpeg)

![](_page_49_Picture_324.jpeg)

#### **Agenda**

- Updates
- Drone and car tests
- Launch Operations

#### **Progress since last meeting**

#### Antoine:

- 3D printed the model of the drone support
- Got the data off the wind tunnel in France
	- $\circ$  Stationary canards with different angles of attack (from 0 degrees to 15 degrees) o Increase the wind speeds by increments of 5m/s up to 40m/s
- Redesigned the transmission system of the Aptos module; currently the canards are not attached properly to the servos

#### Alex Monk:

- Telemetry is not ideal; mostly working in the past as it transmits data; but frequency shifts every time when you turn it on
	- o The oscillator was 4MHz instead of 40Mhz
	- $\circ$  A new oscillator was fit, registers are read correctly, but still does not get the frequency right => prob because the voltage input is not stable enough (it is not stable from Teensy/Power Supply/AAA Batteries), you get a drop in voltage when the current is drawn for the transmission  $\Rightarrow$  get a circuit to speed up the voltage set
		- Order a voltage regulator and some regulators

#### Sam:

• Look into Kalman filter between accelerometer and gyroscope to stop the gyro drift in midflight. Keep this for his report

#### Oliver:

- Further developed the servo driver; got the input as millidegrees
- Initial orientation of the board is worked out using the accelerometer; therefore, board can be initialized on the pad rather than ground
	- o Due to the gyroscope reading; initially gyro was calibrated by lying on flat ground, but we cannot do that on a field.
	- $\circ$  Additionally, when rocket is stationary, remove the gyro drift using the acceleration data (if stationary the acceleration should reveal the orientation of the rocket on pad).
- Currently working on the update of the orientation based on accelerometer
- Try to set the servos to the orientation of the board to see if the Euler angles work, some issue with the char pointer

#### Alex Posta:

- Check the controller code from C that was translate from MATLAB using the hardware: faced multiple issue with the way in which the data was passed from one function to others; the gyroscope data was not calibrating after a time; the servo deflections were not correct angles; look at the servo transmission mechanism->canards are not attached properly
	- o Solve the C pass by reference issues in various functions.
	- $\circ$  Got to the point in which the orientation function outputs some Euler angles and they are passed on the controller to receive servo deflections.
	- o The servo deflections react to yaw/pitch but did not conclude whether the output is correct or not.
- Change the frameArray structure to reflect the new sensors.
	- o FrameArray contains a maximum of 128 bytes
	- $\circ$  Included the majority of the sensors + Euler angle and rates
	- o Need to talk to Ollie to confirm that structure is what is needed; Sam also mentioned two additional variables that he needs

#### **Key notes**

- For Antoine, try to get a mathematical equation for the canards; would be extremely beneficial for the controller in the future
- For Alex Monk, get a voltage regulator fitted; regulator arrives tomorrow (Amazon), another one comes on Monday (Mouser)
- Sam: give us a csv file of the Euler angle / rates / velocity / altitude
- Alex Posta: get the velocity out of barometer; change the NAND flash

Issues:

- Servo 1 works as long as you use it with ID 1 instead of 101
- For csv printing, do not use the equal sign; talk further about the NAND Flash storing procedure (Alex Posta + Ollie)
- Extra 96 bits available on the NAND Flash: Sam needs two values for Roll and Pitch
- Alex needs SPI1 (for telemetry) in mode 0
- Canard deflections: bump them to int16 and change the orientation to use the struct instead of the chart; store it in millidegrees

#### **Actions for next meeting**

#### Drone test:

- Try to do a drone test on Wednesday.
	- $\circ$  If system does not look good, do further drone testing the week after the 14<sup>th</sup>
	- o if weather does not improve by Tuesday, decide whether we want to do the launch
- Total payload test: approx. 500g
	- $\circ$  If needed; fly the telemetry assembly separate from the avionics

#### Tuesday meeting:

• 6:30pm Tuesday; decide what to do this week.

#### **Supervisor signature**

Donyer His

![](_page_51_Picture_216.jpeg)

- Less than 2 weeks to submit
- See group word document for section splits
- Do final tests on Monday: run another vacuum test, try to do a drone test. Telemetry?
- Meet on Wednesday, the 24<sup>th</sup>, to check first draft of all sections for group report; meet at 2pm
- $\bullet$  Late long meeting on the 30<sup>th</sup> of April to submit the group report

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#### **Actions for next meeting**

• Write report

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![](_page_52_Picture_128.jpeg)